Functionally graded adherends by additive manufacturing

M.Q. dos Reis, J. Galante, G.M.F Ramalho, M. Frascio, R.J.C. Carbas, E.A.S. Marques & L.F.M. da Silva



Introduction

The use of adhesive joints and additive manufacturing in the transportation industry can provide several advantages over conventional fabrication methods. A few of these advantages are the ability to easily join different materials with complex shapes, permit the manufacture of stiffer assemblies with a more uniform stress field, create more opportunities for part consolidation that allow for increased design flexibility [1,2]. Single lap joint (SLJ) are the most common configuration used by industries as they are simple to manufacture and are very efficient if loaded in shear, the most preferable loading mode for adhesive joints [3]. One of the major drawbacks associated with these kinds of joints is the stress distribution along the bond line as they tend to exhibit high stress concentration at the ends of overlap length, which can significantly limit joint strength [4]. One of the techniques that could be used to minimize this problem is the use of functionally graded adherends and one way to accomplish this is by using additive manufacturing. This technology as grown immensely in recent years but there are still many unknown variables regarding the material behavior and printing orientations and thus a thorough analysis of many engineering materials and there printing orientations has to be done as a means to allow a flawless integration of additive manufacturing and adhesive joints

Methodology

Numerical Results

A numerical model was developed in Abaqus[®] to predict the failure load and strength on adhesive joints with functionally graded adherends.

Cohesive zone modelling (CZM):

- Adherends: High strength steel (HSS), fibre reinforced polymer (FRP) and transverse graded adherends with different gradient factors.
- Adhesives: 3M Scotch Weld AF-163-2K (epoxy film) and the Nagase Denatite XNR \bullet 6852E-3 by Nagase-ChemteX (epoxy paste).



Figure 1 – Analytical scheme of a functionally graded adherend





 $1 \le n \le \infty$



distribution law for 0 < n < 1





Figure 4 – Detailed parameters used on the CZM analysis





Graded adherends distribution (stiff interface)



Figure 2 – Graded stiffness distribution for flexible and stiff interface with different gradient factors used on CZM

Z min	0*	45*	90*	
Y max	Stance, declaration			

Figure 3 – Graded adherends obtained by additive manufacturing (varying the materials and orientations



Adhesive	AF-163-2K	XNR 6852 E-3
σ (MPa)	46.93	51.50
au (MPa)	46.86	44.90
E (MPa)	1521.87	1728.00
G (MPa)	563.67	665.00
G _{lc} (N/mm)	4.05	9.20
G _{IIc} (N/mm)	9.77	51.00

XNR6852 E-3

Graded (stiff free face) n=0.1 HSS (210 GPa) Graded (stiff free face) n=1 S Graded (flexible free face) n=0.1 = Graded (flexible free face) n=1 Graded (stiff free face) n=10 Graded (flexible free face) n=10 FRP (30 GPa)

Figure 6 – Failure loads obtained for both adhesives with homogenous and graded adherends for several compositional distribution factors

References

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Conclusions

Additive manufacturing opens windows for fabrication of many geometries and ideas that could not be done before. There is a significant limitation in material properties depending on printing direction and layer lines directions that cause a 3d print to be considered anisotropic. In this paper each possible printing direction was tested and possible graded joints were proposed with simulations to validate the results. This thorough comparison allows for a better understanding when designing 3d printed parts and allows for future single lap joints to be 3d printed with a minimization in stress lines by using multiple materials and the properties of 3d printing directions.



